

Environmental & Earth Sciences GT-1 Sustainable Infrastructure Solutions Geophysical Solutions

June 5, 2024 Job No. 24-0017

Little Rock Port Authority 10600 Industrial Harbor Drive Little Rock, Arkansas 72206

Attn: Mr. Bryan Day

# RE: INTERIM RESULTS - GEOTECHNICAL INVESTIGATION LITTLE ROCK INDUSTRIAL PORT 1000+ ACRE SITE LITTLE ROCK, PULASKI COUNTY, ARKANSAS

### **INTRODUCTION**

This interim report presents the initial results of the geotechnical feasibility investigation being performed for the 1000+ acre site at the Little Rock Industrial Port in Little Rock, Arkansas. These services were authorized on behalf of the Little Rock Port Authority by Mr. Bryan Day on January 19, 2024. This study is being performed in general accordance with our proposal of November 28, 2023 (GHBW Proposal 23-072). The field studies have been performed as permitted by landowner access permission and weather-related site access.

We understand that the subject site is a potential development or developments on an approximately 1000-acre site. The site includes multiple tracts at the Little Rock Industrial Port, southwest of the Welspun Pipes facility and north of Harper Road. Currently, the project site is a mixture of open pasture, crop and grass fields, and stands of trees. Specific information on site layout and development structures or details has not been developed at this time.

#### SUBSURFACE EXPLORATION

Subsurface conditions have been explored to date by drilling four (4) sample borings to depths of 60 to 85 feet. The site vicinity is shown on Plate 1. The approximate locations of the completed borings are shown on the Plan of Borings, Plate 2. Preliminary boring logs, presenting descriptions of the subsurface strata encountered and results of field and completed laboratory tests, are included as Plates 3 through 8. The approximate ground surface elevation, as inferred from available, published topographic information, is also shown on the logs. It must be recognized that the elevations shown are approximate and actual elevations may vary. A key to the terms and symbols used on the logs is presented as Plate 9.

The borings were drilled with a track-mounted CME-55 rotary-drilling rig using a combination of dry-auger and rotary-wash drilling procedures. Samples were typically obtained using a 2-inch-diameter split-barrel sampler driven into the strata by blows of a 140-lb automatic hammer dropped 30 inches, in accordance with Standard Penetration Test (SPT) procedures. The number of blows required to drive the standard split-barrel sampler the final 12 inches of an 18-inch total drive, or portion thereof, is defined as the Standard Penetration Number (N). Recorded N-values are shown on the boring logs in the "Blows Per Ft" column.



Selected undisturbed samples of cohesive soils were obtained using a 3-in.-diameter thinwalled tube hydraulically advanced into the soil. Undrained shear strength of the cohesive soils was estimated in the field using a calibrated hand penetrometer. Estimated shear strength values are plotted on the log forms, in tons per sq ft, as circles enclosing an "x".

All samples were removed from sampling tools in the field, examined and visually classified by the field geologist. Samples were then placed in appropriate containers to prevent moisture loss and/or change in condition during transfer to our laboratory for further examination and testing.

The borings were advanced using dry-auger drilling procedures to the extent possible to facilitate groundwater observations. Observations regarding groundwater are noted in the lower-right portion of each log and are discussed in subsequent sections of this report.

The results of completed laboratory tests are shown on the logs at the appropriate depth. The water contents are plotted in accordance with the scale and symbols contained in the legend in the upper-right portion of the log forms. The Atterberg limits test results are plotted on the boring logs as pluses connected with a dashed line using the water content scale. The percent of soil passing through the No. 200 sieve is noted in the "Minus No. 200" column on the appropriate log forms.

# **GENERAL SITE and SUBSURFACE CONDITIONS**

### Site Conditions

The project site areas drilled to date are located south of Thibault Road and the Welspun Tubular plant at the Little Rock Industrial Port in Little Rock, Arkansas. The site is presently open and undeveloped. The open site has a mixed ground surface cover predominantly comprised of fallow fields, agricultural tracts, high weeds, crops, and scattered areas of mature trees. The surrounding properties are composed of a similar mixture of open fields, cropland, and scattered trees. The Arkansas River is located to the east, with a wetlands area and an existing flood control levee. A prominent drainage ditch extends southwest from the intersection of Thibault Road and Frazier Pike, turning west about 2700 ft south of the east-west roadway alignment. Some wooded and wet areas are locally on the north side of the ditch. Ditches are common along roadways to facilitate surface drainage. The site terrain is predominantly flat. Surface water drainage is considered very poor to poor.

### Site Geology

The project location is in the Mississippi Embayment Geophysical Province. The surface geology of this location is Recent (Quaternary) Alluvium of the Arkansas River flood plain. The alluvium is typically comprised of a mixture of silt, sandy silt, silty clay and clay with silty sand and sand at depth, a mixture of clastic materials eroded from upstream locations. The alluvium in the area is typically underlain by Tertiary deposits and locally by igneous rocks of a Cretaceous intrusion. Bedrock (Paleozoic rock) in this location is reported to be in excess of 200- to 300-ft depth.

### Seismic Conditions

The Pulaski County, Arkansas site is located in Seismic Zone 1, noted by the Arkansas Building Authority (2005) as the zone of least anticipated seismic potential. The results of the completed borings and relevant borings from adjacent sites have been utilized to determine the seismic site class in accordance with the criteria of the Arkansas Fire Prevention Code Vol II and the International Building Code 2021 / ASCE 7-16. To supplement data on subsurface conditions at depths in excess of the maximum 85-ft exploration depths of the borings performed for this study phase, the results of prior borings near this location have been utilized.



Based on IBC 2021 and ASCE 7-16, a Seismic Site Class D (stiff soil profile) has preliminarily been determined. Preliminary liquefaction analyses have been performed to evaluate the liquefaction potential of the foundation soils. The analysis was performed utilizing the methodology and procedures proposed by Idriss and Boulanger<sup>1</sup> in 2008. For the purpose of liquefaction analysis, an earthquake Moment Magnitude (M<sub>w</sub>) of 6.0 was utilized. This earthquake magnitude is roughly equivalent to a Modified Mercalli Intensity of VII, i.e., a very strong earthquake with general alarm and cracking of walls. The results of the preliminary liquefaction analyses are summarized in Attachment 1.

The preliminary liquefaction analysis results indicate a low potential for liquefaction triggering. It should be recognized the liquefaction potential may vary across the relatively large site area.

### Subsurface Conditions

The results of the four (4) borings drilled at this time indicate that the surface and near-surface soils are comprised of very loose to medium dense silt, fine sandy silt, and silty fine sand to 13- to 15-ft depth. These fine-grained soils typically have low plasticity with very low to low shear strength and moderate to high compressibility. The predominantly silty soil units contain interbedded, localized and discontinuous seams, layers, and strata of clay and silty clay.

The upper silty soil units are underlain by very soft to stiff clay and silty clay strata to variable depths of 23- to 28-ft depth. The clay and silty clay units vary in thickness, consistency, and depth intervals. However, these clayey soils typically have low strength and moderate to high compressibility. Plasticity ranges from medium to high. The potential for shrink-swell activity is considered low due to the high *in-situ* water content and the depths of these units.

The clayey soils are typically underlain below about 23- to 28-ft depth by medium dense to very dense fine sand, silty fine to medium sand, and fine to coarse sand. This stratum generally grades from slightly silty fine-grained sand to increasingly medium to coarse sand and decreasing silt content. Relative density increases with depth and compressibility decreases.

Groundwater was encountered at 1.5 to 13 ft below existing grades in May 2024. The shallow water at 1.5 ft is considered localized perched groundwater associated with surface water infiltration. It is our experience that the groundwater levels at 12 to 13 ft are more typical of the Port area. Groundwater levels will vary with seasonal precipitation and surface runoff and infiltration.

### Significant Conditions

The site and subsurface conditions considered significant to design and construction of structures and infrastructure on this site are summarized below.

- a) The flat site terrain with poor to very poor surface water drainage.
- b) The surficial moisture-sensitive silt and sandy silt commonly at the ground surface which will be subject to significant strength and stability reductions during wet seasons.
- c) The predominant low shear strength and high to moderate compressibility of the onsite soils to 23- to 28-ft depth.

<sup>&</sup>lt;sup>1</sup> "Soil Liquefaction during Earthquakes." Earthquake Engineering Research Institute, MNO-12, Idriss and Boulanger, 2008.



- d) The increase in shear strength and decrease in compressibility below 23- to 28-ft depth.
- e) The presence of localized perched water at shallow depths on the order of 1.5 ft but more typical groundwater levels at 12- to 13-ft depth in May 2024.
- f) The results of preliminary analyses indicating a Seismic Site Class D and a low potential for liquefaction triggering.

## **CLOSURE**

This interim report has been prepared to provide preliminary information regarding site and subsurface conditions on the 1000+ acre site. The conclusions and comments contained herein have been developed based on a discrete number of widely spaced sample borings. This information is intended for general information and use in feasibility planning and conceptual design only. Final design recommendations must be based on an appropriate geotechnical study utilizing specific site grading plans, building layout, and structure loading information. We are available to assist with providing an appropriate scope of work for the final geotechnical investigation as plans are more developed.

The following illustrations are attached and complete this preliminary report.

P	late 1		Site Vicinity
P	late 2		Plan of Borings
P	lates 3 through 8		Preliminary Boring Logs
P	late 9		Key to Terms and Symbols
А	ttachment 1		Results of Preliminary Liquefaction Analysis
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We appreciate the opportunity to provide preliminary results and recommendations for this project. Please contact us should you have any questions regarding this information. In the meantime, we will be working on the final report.

Sincerely,

GRUBBS, HOSKYN, BARTON & WYATT, LLC

Mark E. Wyatt, P.E. President

MEW:jw

Copies submitted:

Little Rock Port Authority Attn: Mr. Bryan Day

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